

Part – 1 :

Q(1):

I don't have the exact question, but it was something like this:

What makes airplanes go up (fly)?

Answer:

Due to the difference in the air speed above and below the wing of the airplane, where the speed above is higher than below, creating less pressure above the wing as compared to the pressure below. The difference in pressure creates uplift force.

Q(2):

What is the minimum runway blast pad width in meters for a design aircraft C-IV (answer format: one digit to the right of the decimal point, e.g. 255.0)

Answer: 60.0

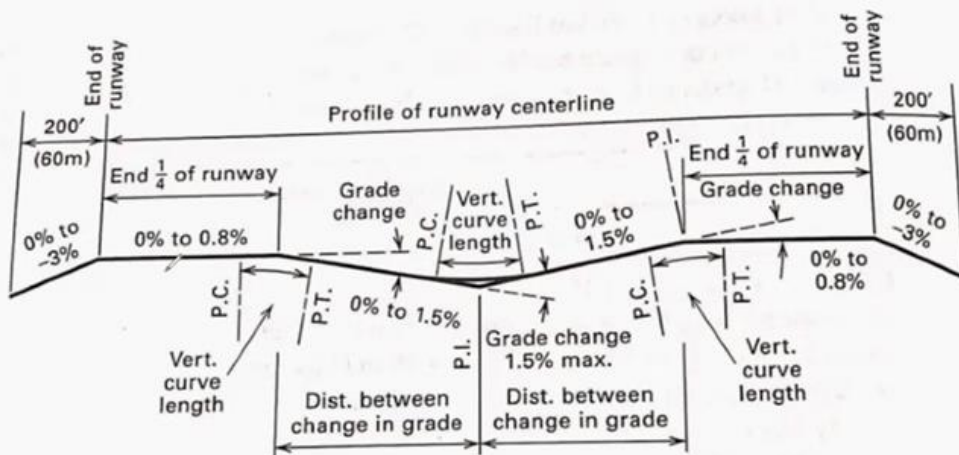
Table 18-5 Runway Design and Separation Standards for Aircraft Approach Categories C & D

| Item | Airplane Design Group | | | | | |
|---|-----------------------|-------------------|-------------------|-------------------|-------------------|-------------------|
| | I | II | III | IV | V | VI |
| Runway Width | 100 ft 30 m | 100 ft 30 m | 100 ft 30 m | 150 ft 45 m | 150 ft 45 m | 200 ft 60 m |
| Runway Shoulder Width | 10 ft 3 m | 10 ft 3 m | 20 ft 6 m | 25 ft 7.5 m | 35 ft 10.5 m | 40 ft 12 m |
| Runway Blast Pad Width | 120 ft 36 m | 120 ft 36 m | 140 ft 42 m | 200 ft 60 m | 220 ft 66 m | 280 ft 84 m |
| Runway Blast Pad Length | 100 ft 30 m | 150 ft 45 m | 200 ft 60 m | 200 ft 60 m | 400 ft 120 m | 400 ft 120 m |
| Runway Safety Area Width | 500 ft 150 m | 500 ft 150 m | 500 ft 150 m | 500 ft 150 m | 500 ft 150 m | 500 ft 150 m |
| Runway Safety Area Length Beyond RW End | 1,000 ft 300 m | 1,000 ft 300 m | 1,000 ft 300 m | 1,000 ft 300 m | 1,000 ft 300 m | 1,000 ft 300 m |
| Runway Object Free Area | 800 ft | 800 ft | 800 ft | 800 ft | 800 ft | 800 ft |

Q(3):

What is the minimum length of vertical curve in meters for a design aircraft D-IV given the tangents at the PVI are minus 0.75% and plus 0.75% (answer format: whole numbers without decimal point and rounded to a whole number, e.g. 175)

Answer: 450



Minimum distance between change in grade = 1000' (300m) · sum of grade changes (in percent).

Minimum length of vertical curves = 1000' (300m) · grade change (in percent).

Figure 18-3b Longitudinal grade limitations for aircraft approach categories C and D. (Source: Airport Design, FAA Advisory Circular 150/5300-13, Changes 1-4, September 29, 1989.)

$$\text{min Length of Vertical Curve} = 300(0.75 + 0.75) = 450 \text{ m}$$

Q(4):

Give the magnetic azimuth of single runway is 76, what are runway numbers of this runway for each of the two ends of runway (answer format: whole numbers with no decimal point and symbol and "&" between the two numbers with no spaces before or after the "&", e.g., 2&13)

Answer: 8 & 26

$$76 \approx 80 \text{ (Rounded to nearest 10)}$$

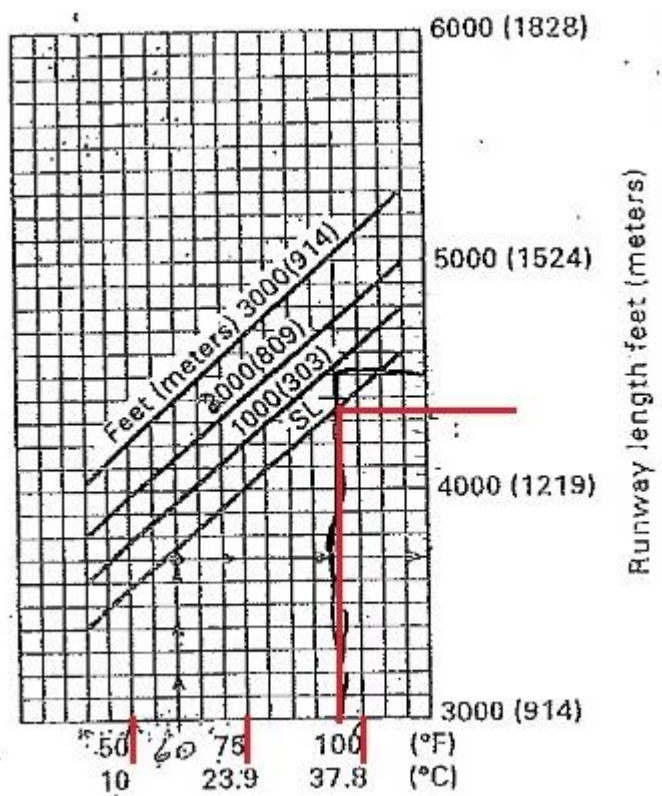
$$\text{First Number} = \frac{80}{10} = 8$$

$$\text{Second Number} = 8 + 18 = 26$$

Q(5):

What is the required runway length of a design aircraft of Beech B99 at location with elevation at sea level and mean daily maximum temperature of the hottest month of the year is 95 degree Fahrenheit (answer in whole numbers without decimal point and rounded to upper/higher 100ft, e.g. 2200)

Answer: 4300



Q(6):

Given expected daily traffic in the table below, determine the IFR hourly capacity for runway configuration number 4 in table 16.3, p. 519 in the textbook (answer format: whole number without decimal point, e.g., 98)

| Aircraft type | Expected typical daily number of aircrafts |
|---|--|
| Class A: Small single-engine aircrafts 12,500lb or less | 40 |
| Class B: Small multiengine aircrafts, 12,500lb or less and learjets | 60 |
| Class C: large aircrafts, 12,500lb an up to 300,000lb | 80 |
| Class D: heavy aircraft, more than 300,000lb | 20 |

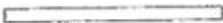



Answer: **56**

$$\%C = \frac{80}{40 + 60 + 80 + 20} * 100\% = 40\%$$

$$\%D = \frac{20}{40 + 60 + 80 + 20} * 100\% = 10\%$$

$$\text{Mix Index} = \%C + 3(\%D) = 40 + 3(10) = 70$$

Table 16-3 Airport Capacities for Long-Range Planning Purpose

| Runway Use Configuration | Mix Index (C + 3D) | Hourly (hr) Capacity (Operations) | | Annual Service Volume (Operations/yr) |
|--|--------------------|-----------------------------------|-----|---------------------------------------|
| | | VFR | IFR | |
| 1.  | 0-20 | 98 | 59 | 230,000 |
| | 21-50 | 74 | 57 | 195,000 |
| | 51-80 | 63 | 56 | 205,000 |
| | 81-120 | 55 | 53 | 210,000 |
| | 121-180 | 51 | 50 | 240,000 |
| 2.  | 0-20 | 197 | 59 | 355,000 |
| | 21-50 | 145 | 57 | 275,000 |
| | 51-80 | 121 | 56 | 260,000 |
| | 81-120 | 105 | 59 | 285,000 |
| | 121-180 | 94 | 60 | 340,000 |
| 3.  | 0-20 | 295 | 62 | 385,000 |
| | 21-50 | 219 | 63 | 310,000 |
| | 51-80 | 184 | 65 | 290,000 |
| | 81-120 | 161 | 70 | 315,000 |
| | 121-180 | 146 | 75 | 385,000 |
| 4.  | 0-20 | 98 | 59 | 230,000 |
| | 21-50 | 77 | 57 | 200,000 |
| | 51-80 | 77 | 56 | 215,000 |
| | 81-120 | 76 | 59 | 225,000 |
| | 121-180 | 72 | 60 | 265,000 |

Q(7):

Airport demand for passenger transfers depends mainly on

- a. Population and level of education
- b. Population and production of goods
- c. Population and being a hub airport
- d. Using the airport as a hub airport by airlines
- e. Population and economic character

But not sure, it might be (c) though!! You will have to ask Dr. Faisal.

Q(8):

In table 16.2, p.511 of the textbook, the percentage of wind in the study period in the range of 3.500 to 6.499 knots in the direction of between azimuths of 315 and 325 is (answer format: two digits to the right of the decimal point with no "%" sign, e.g., 1.42)

Answer: 0.97

16-6. Runway Orientation 511

Table 16-2 Typical Wind Data
Hourly Observations of Wind Speed (Knots)

| Direction | Wind Speed (Knots) | | | | | | | | Total |
|-----------|--------------------|-------|-------|-------|-------|-------|-------|---------|-------|
| | 4-6 | 7-10 | 11-16 | 17-21 | 22-27 | 28-33 | 34-40 | 41 Over | |
| 1 | 469 | 842 | 568 | 212 | 0 | 0 | 0 | 0 | 2091 |
| 2 | 568 | 1263 | 820 | 169 | 0 | 0 | 0 | 0 | 2820 |
| 3 | 294 | 775 | 519 | 73 | 0 | 0 | 0 | 0 | 1670 |
| 4 | 317 | 872 | 509 | 9 | 0 | 0 | 0 | 0 | 1771 |
| 5 | 268 | 861 | 437 | 62 | 11 | 0 | 0 | 0 | 1672 |
| 6 | 357 | 534 | 151 | 106 | 0 | 0 | 0 | 0 | 1092 |
| 7 | 369 | 403 | 273 | 42 | 8 | 0 | 0 | 0 | 1175 |
| 8 | 158 | 261 | 138 | 84 | 36 | 10 | 0 | 0 | 814 |
| 9 | 167 | 352 | 176 | 69 | 73 | 52 | 41 | 22 | 971 |
| 10 | 119 | 303 | 127 | 180 | 68 | 59 | 21 | 0 | 877 |
| 11 | 323 | 586 | 268 | 312 | 98 | 41 | 9 | 0 | 1651 |
| 12 | 618 | 1397 | 624 | 779 | 271 | 23 | 28 | 0 | 3779 |
| 13 | 472 | 1375 | 674 | 531 | 271 | 69 | 21 | 0 | 3571 |
| 14 | 647 | 1377 | 574 | 281 | 452 | 67 | 0 | 0 | 3008 |
| 15 | 338 | 1093 | 348 | 135 | 27 | 0 | 0 | 0 | 1941 |
| 16 | 560 | 1399 | 523 | 121 | 19 | 0 | 0 | 0 | 2622 |
| 17 | 587 | 883 | 469 | 128 | 12 | 0 | 0 | 0 | 2079 |
| 18 | 1046 | 1984 | 1068 | 297 | 83 | 18 | 0 | 0 | 4496 |
| 19 | 499 | 793 | 586 | 241 | 92 | 0 | 0 | 0 | 2211 |
| 20 | 371 | 946 | 615 | 243 | 64 | 0 | 0 | 0 | 2239 |
| 21 | 340 | 732 | 528 | 323 | 147 | 8 | 0 | 0 | 2078 |
| 22 | 479 | 768 | 603 | 231 | 115 | 38 | 19 | 0 | 2253 |
| 23 | 187 | 1008 | 915 | 413 | 192 | 0 | 0 | 0 | 2715 |
| 24 | 458 | 943 | 800 | 453 | 96 | 11 | 18 | 0 | 2779 |
| 25 | 351 | 899 | 752 | 297 | 102 | 21 | 9 | 0 | 2431 |
| 26 | 368 | 731 | 379 | 208 | 53 | 0 | 0 | 0 | 1739 |
| 27 | 411 | 748 | 469 | 232 | 118 | 19 | 0 | 0 | 1997 |
| 28 | 191 | 554 | 276 | 287 | 118 | 0 | 0 | 0 | 1426 |
| 29 | 271 | 642 | 548 | 479 | 143 | 17 | 0 | 0 | 2100 |
| 30 | 379 | 873 | 526 | 543 | 208 | 34 | 0 | 0 | 2563 |
| 31 | 299 | 643 | 597 | 618 | 222 | 19 | 0 | 0 | 2398 |
| 32 | 397 | 852 | 521 | 559 | 158 | 23 | 0 | 0 | 2510 |
| 33 | 236 | 721 | 324 | 238 | 48 | 0 | 0 | 0 | 1567 |
| 34 | 280 | 916 | 845 | 307 | 24 | 0 | 0 | 0 | 2372 |
| 35 | 252 | 931 | 918 | 487 | 23 | 0 | 0 | 0 | 2611 |
| 36 | 501 | 1568 | 1381 | 569 | 27 | 0 | 0 | 0 | 4046 |
| 0 | 7729 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7729 |
| TOTAL: | 21676 | 31828 | 19849 | 10437 | 3357 | 529 | 166 | 22 | 87864 |

Source: Airport Design, FAA Advisory Circular 150/5300-13, including Changes 1-4, Federal Aviation Administration, Washington, DC, September 29, 1989.

$$\text{Wind(\%)} = \frac{852}{87864} * 100\% = 0.97\%$$

Q(9): Don't have it, couldn't even open it, ITC crashed back then!!.

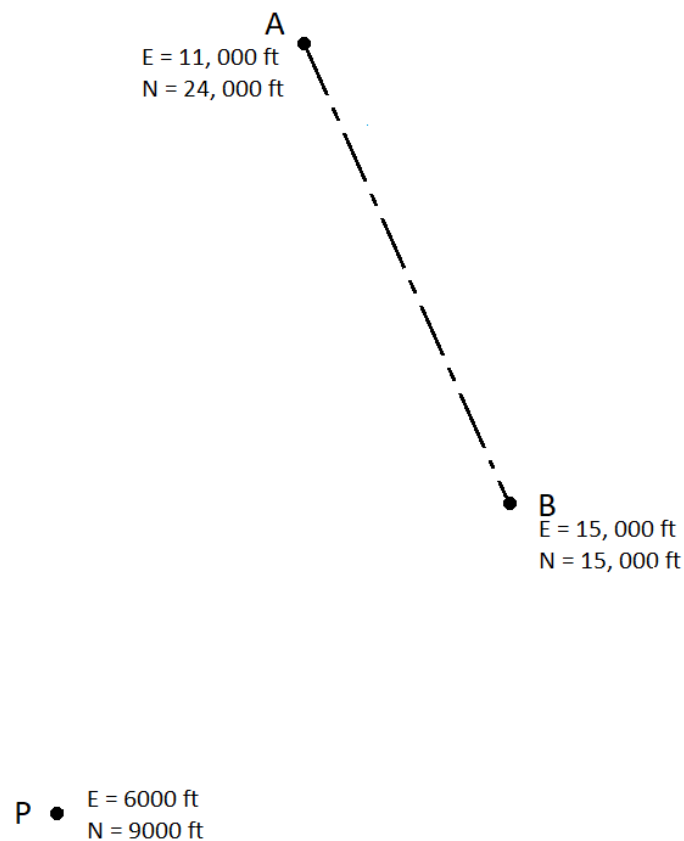
Part – 2

Question 1: (30 marks) – No groups for this question, entire class one group

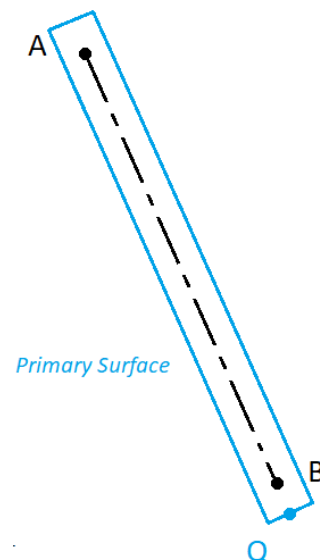
Given an airport with one precision instrument runway. The ends of the runway centerline have the following coordinates (N: 15000', E: 15000') and (N: 24000', E: 11000'). The airport-established elevation is 760' above msl.

Determine the maximum height of a structure at a proposed construction site with the following coordinates (N: 9000', E: 6000', Z: 730' above msl) according to the FAA imaginary surfaces standards

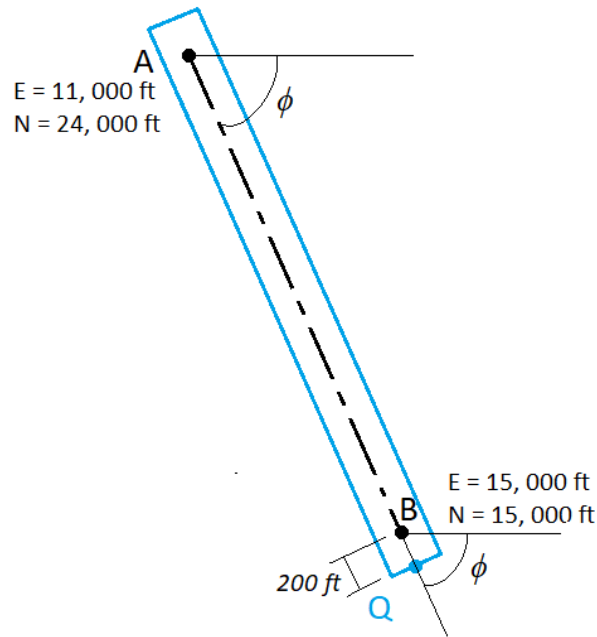
Note: all coordinates in feet



For Group 1:



We must find the coordinates of point (Q) to do this we first must find the angle ϕ :

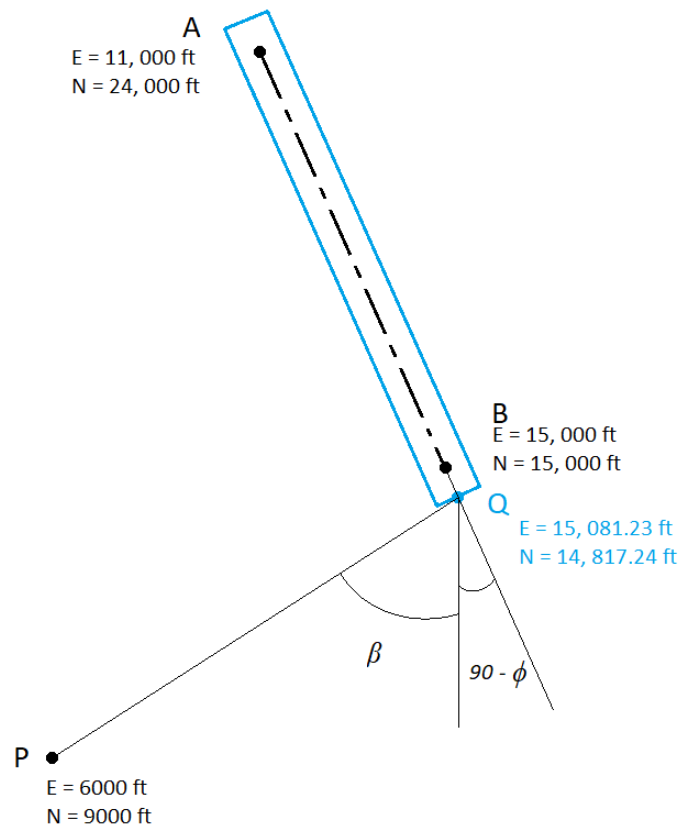


$$\phi = \tan^{-1} \left(\frac{24,000 - 15,000}{15,000 - 11,000} \right) = 66.0375^\circ$$

$$E_Q = E_B + 200 \cos(\phi) = 15,000 + 200 \cos(66.0375) = 15,081.23 \text{ ft}$$

$$N_Q = N_B - 200 \sin(\phi) = 15,000 - 200 \sin(66.0375) = 14,817.24 \text{ ft}$$

We must check the angle between the Runway CL and the line QP (to know if more or less than 90°):

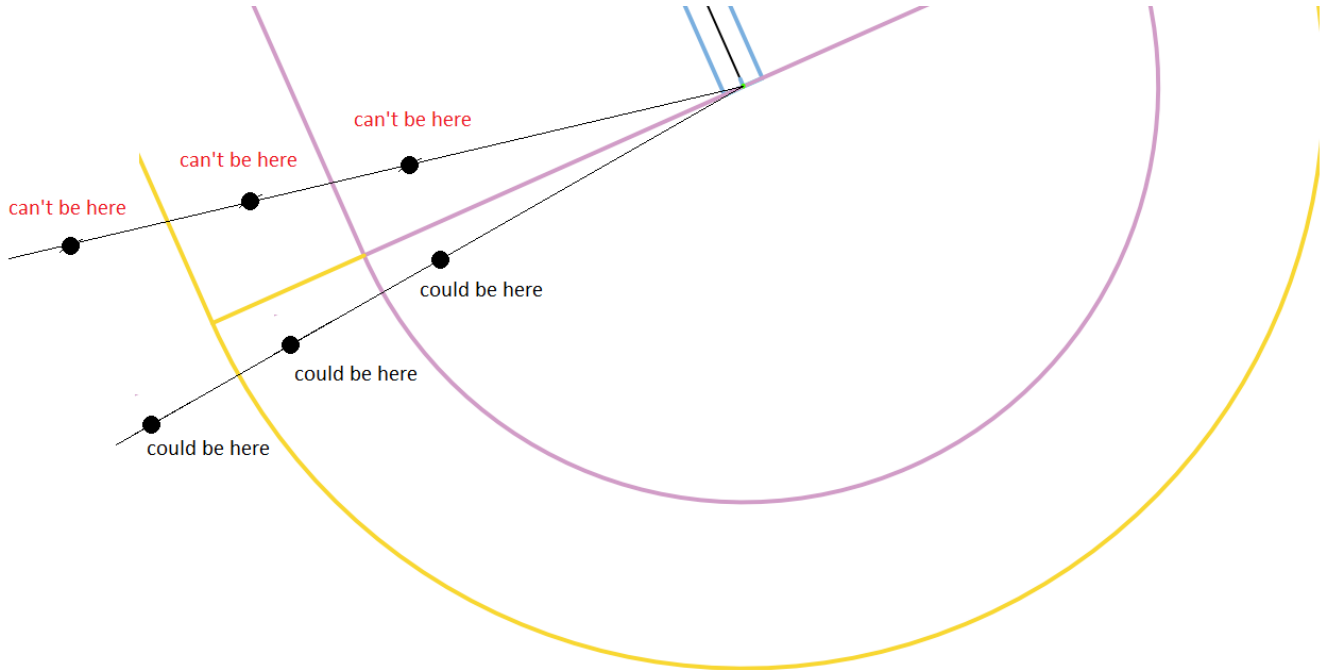


$$90^\circ - \phi = 90^\circ - 66.0375^\circ = 23.9625^\circ$$

$$\beta = \tan^{-1} \left(\frac{15,081.23 - 6000}{14,817.24 - 9000} \right) = 57.3573^\circ$$

$$\beta + (90 - \phi) = 57.3573 + 23.9625 = 81.32^\circ < 90$$

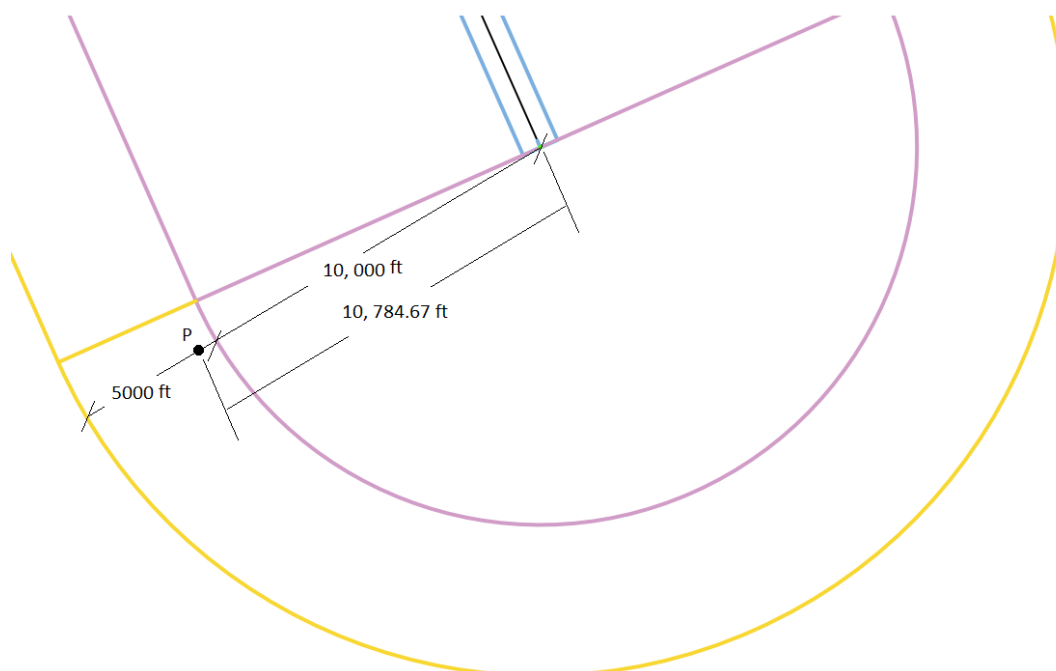
Since the angle is $< 90^\circ$ the site point (P) might be in one of the following positions:



To determine which position, we must find the radius (R') which is the line QP:

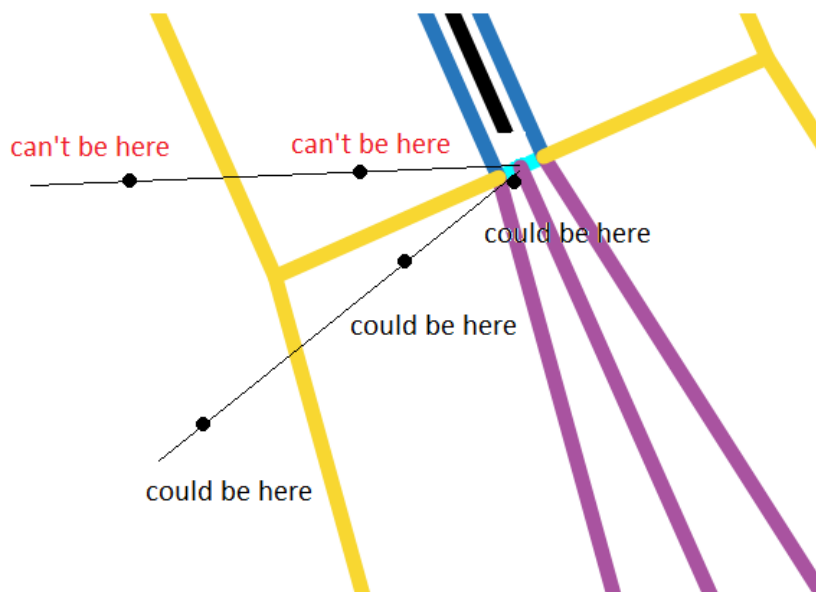
$$R' = \sqrt{(15,081.23 - 6000)^2 + (14,817.24 - 9000)^2} = 10,784.67 \text{ ft}$$

$10,000 < R' < 15,000 \Rightarrow$ The site Point (P) is within the **Conical Surface** for group 1



Group 2:

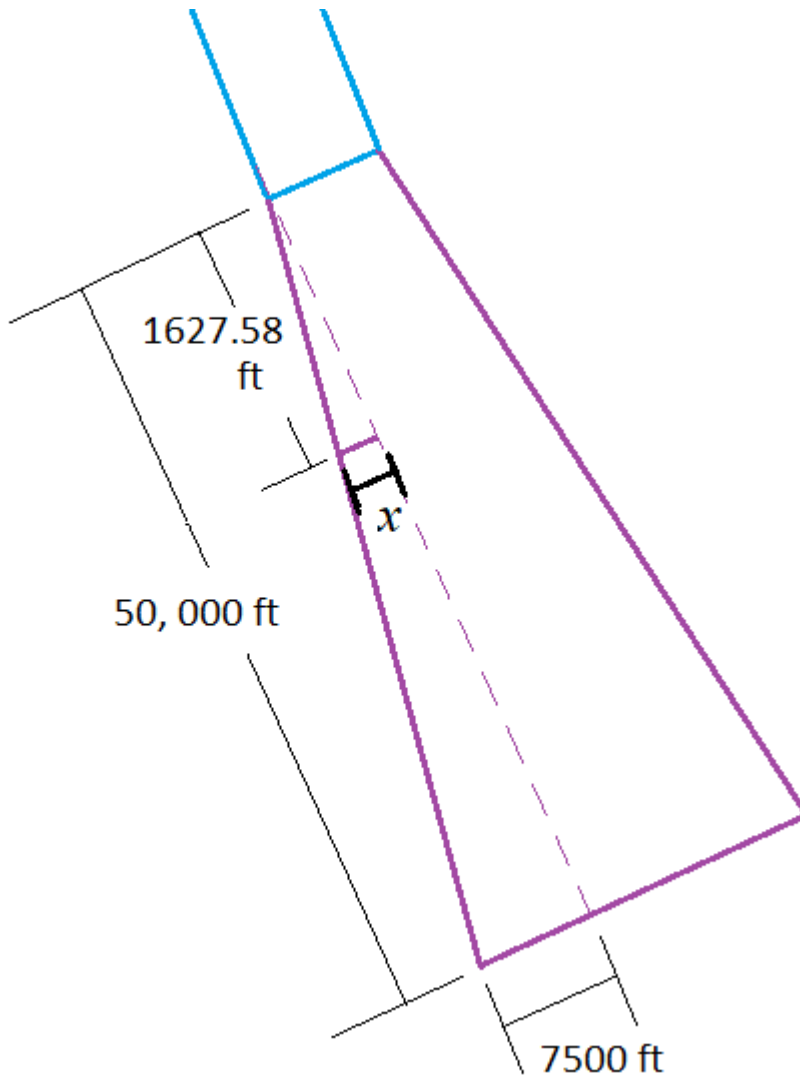
Since the angle between CL & QP $< 90^\circ$ the point might be in one of these positions:



In order to determine the exact position, we must find the component of QP parallel to CL and the component of QP perpendicular to CL:

$$QP_{\perp} = R' \sin(\beta + (90^\circ - \phi)) = 10,784.67 \sin(81.32^\circ) = 10,661.15 \text{ ft}$$

$$QP_{\parallel} = R' \cos(\beta + (90^\circ - \phi)) = 10,784.67 \cos(81.32^\circ) = 1627.58 \text{ ft}$$



by similar triangles:

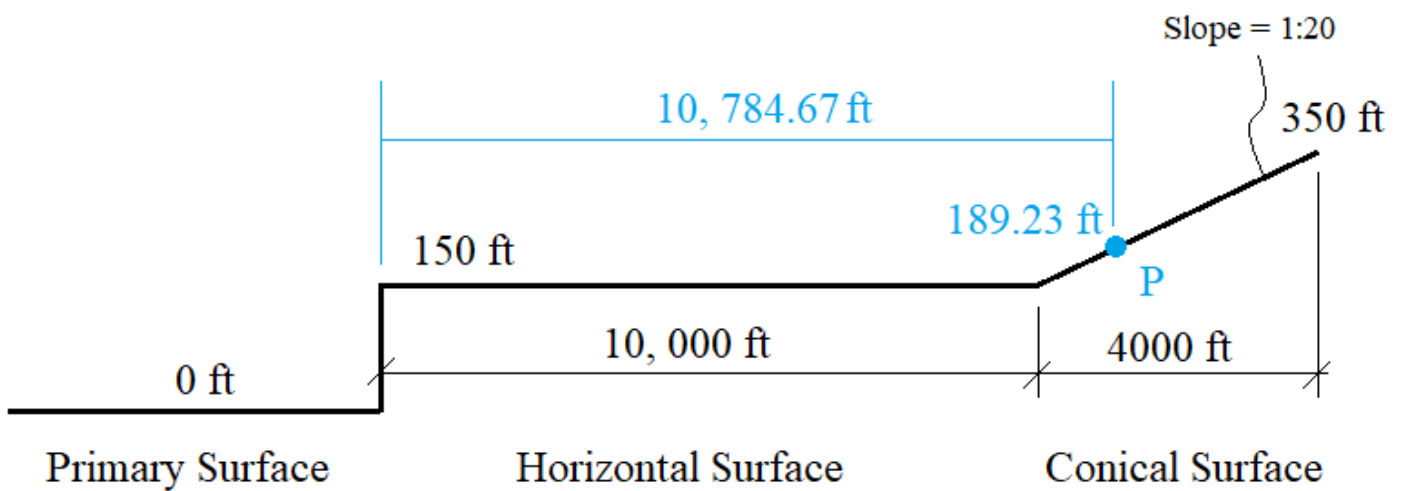
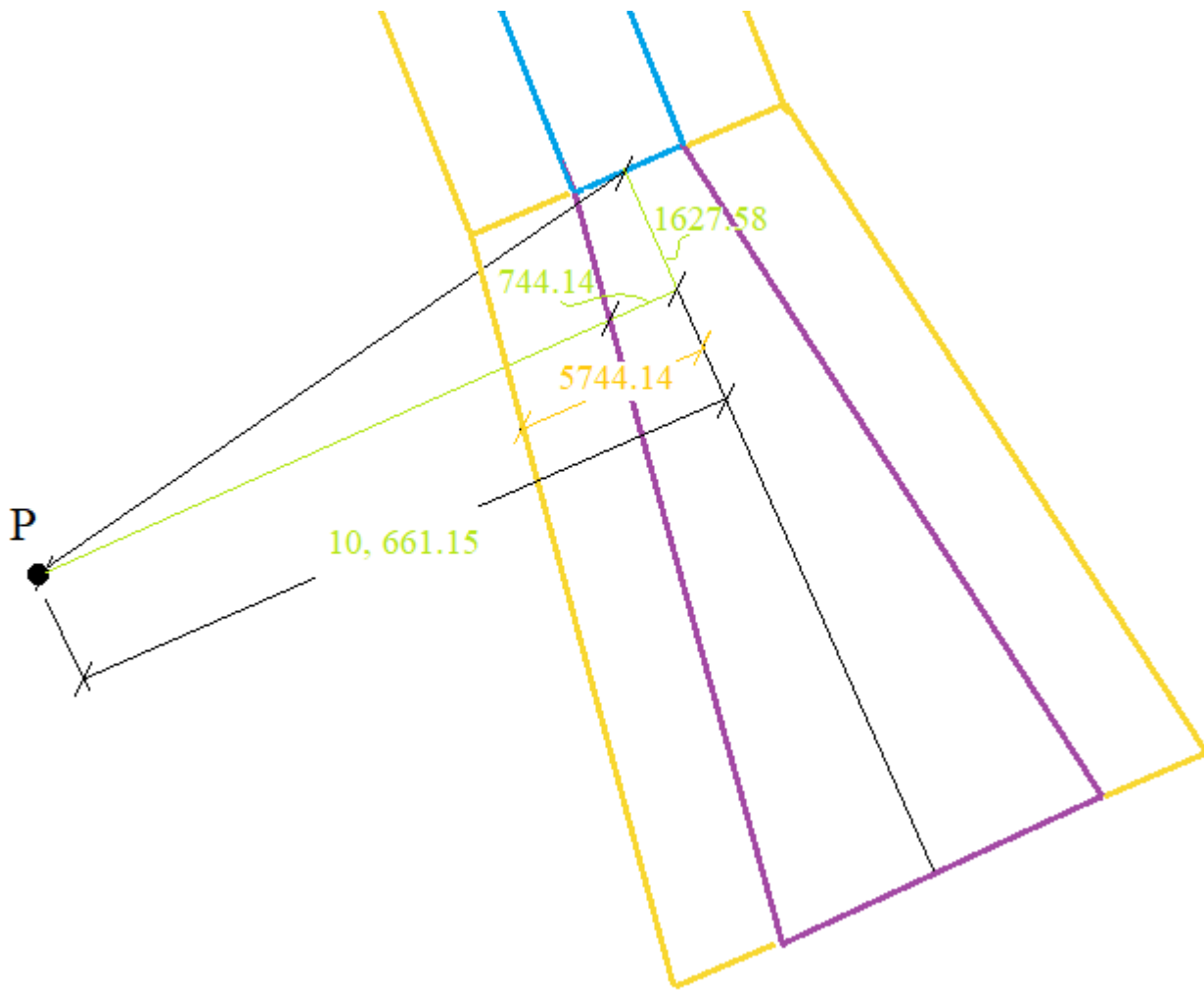
$$x = 1627.58 \left(\frac{7500}{50,000} \right) = 244.1365 \text{ ft}$$

distance to boundary of Approach Surface = $244.1365 + 500 = 744.1365 \text{ ft}$

distance to boundary of Transitional Surface = $744.1365 + 5000 = 5744.1365 \text{ ft}$

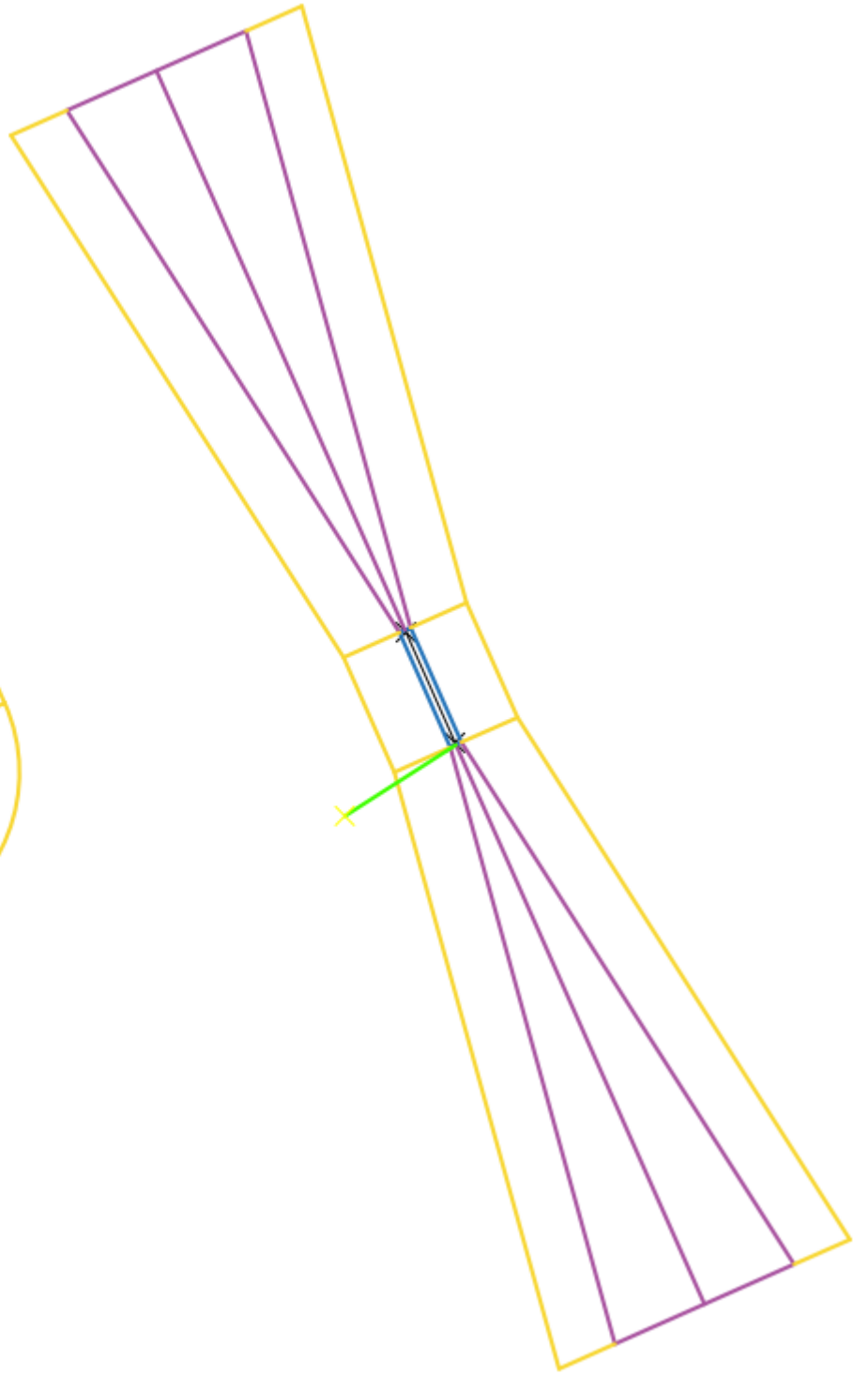
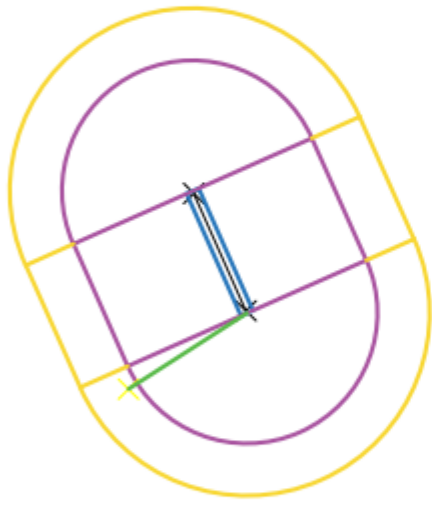
$744.1365 \text{ ft} < 5744.1365 \text{ ft} < (QP_{\perp} = 10,661.15 \text{ ft}) \Rightarrow P, \text{ is not within group 2}$

So, the site point (P) is only controlled by the conical surface of group1, and not limited by group 2:



$$\text{Max Elev. Difference} = 150 + \frac{10,784.67 - 10,000}{4000} = 189.23 \text{ ft}$$

$$\text{Max height of structure} = \text{Max Elev. diff} + \text{Elev}_{R.W} - \text{Elev}_P = 189.23 + 760 - 730 = 219.23 \text{ ft}$$



Question 2: (10 marks)

Group D: Digit 5 and 6 from the left of students numbers 75 - 99 inclusive (e.g., 1171879)

Table below provides the expected average number of aircraft arrival per day for four category of aircrafts with expected mean time gate occupancy for each category; estimate the number of required gates according to European traffic.

| Aircraft category | Average number of aircraft arrivals per hour | Mean time gate occupancy in minutes |
|-------------------|--|-------------------------------------|
| A | 3 | 45 |
| B | 17 | 55 |
| C | 20 | 65 |
| C | 25 | 75 |

$$n = m \left(\frac{\text{Aircrafts}}{\text{hr}} \right) \cdot q \cdot t(\text{hr})$$

$$q = \frac{3 + 17 + 20 + 25}{m} = \frac{65}{m}$$

$$t = \frac{(3)(45) + (17)(55) + (20)(65) + (25)(75)}{(3) + (17) + (20) + (25)} = 65.308 \text{ min} = 1.088 \text{ hr}$$

$$n = m \left(\frac{65}{m} \right) (1.088) = 70.75 = 71 \text{ gates required}$$

Question 3: (20 marks)

Group C: Digit 5 and 6 from the left of students numbers 75 - 99 and 00-09 inclusive (e.g., 1171099)

Given a design B757 aircraft for runway length requirement (similar to table 18.1 & 18.2). The airport is at an elevation of 1000 meters and normal maximum temperature of the hottest month of the year is 28 degrees. Maximum operational take-off weight is 95000kg, and maximum operational landing weight is 195000lb. Determine the required runway length assuming the difference between the highest and lowest points on the runway centerline is 4.5 meters.

For Landing:

Max allowable landing weight = 89,800 kg

Available Landing weight = 195,000 lb = 88,450 Kg

$$W_{Avail} < W_{Max} \Rightarrow (OK)$$

Table 18-1 Runway Length Table: Aircraft Performance, Landing (Boeing 757-232 Series) PW 2037 Engine, 25° Flaps

| Temperature (°C) | By Airport Elevation in Meters | | | | | |
|------------------|--|-------|--------|--------|--------|--------|
| | 0 m | 500 m | 1000 m | 1500 m | 2000 m | 2500 m |
| | ✓ Maximum Allowable Landing Weight (1000 kg) | | | | | |
| 10 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 |
| 12 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 |
| 14 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 |
| 16 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 |
| 18 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 |
| 20 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 |
| 22 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 |
| 24 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 |
| 26 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 |
| 28 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 |
| 30 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 |
| 32 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 |
| 34 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 |
| 36 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 | 89.0 |
| 38 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 | 86.9 |
| 40 | 89.8 | 89.8 | 89.8 | 89.8 | 89.8 | 84.9 |
| 42 | 89.8 | 89.8 | 89.8 | 89.8 | 87.5 | 82.9 |
| 44 | 89.8 | 89.8 | 89.8 | 89.8 | 85.2 | 81.0 |

Runway Length for landing:

Airport Elev. = 1000 m = 3280ft

3000 ft \Rightarrow 6.28

4000 ft \Rightarrow 6.45

3280 ft \Rightarrow ??

| Weight (1000 lb) | By Airport Elevation in Feet | | | | | | | | |
|---------------------|------------------------------|---------|---------|---------|---------|---------|---------|---------|---------|
| | 0 ft | 1000 ft | 2000 ft | 3000 ft | 4000 ft | 5000 ft | 6000 ft | 7000 ft | 8000 ft |
| | Runway Length (1000 ft) | | | | | | | | |
| 125 | 3.65 | 3.72 | 3.79 | 3.85 | 3.92 | 3.98 | 4.05 | 4.11 | 4.18 |
| 130 | 3.89 | 3.96 | 4.04 | 4.12 | 4.21 | 4.30 | 4.39 | 4.49 | 4.60 |
| 135 | 4.08 | 4.17 | 4.26 | 4.35 | 4.45 | 4.56 | 4.67 | 4.80 | 4.94 |
| 140 | 4.24 | 4.33 | 4.43 | 4.54 | 4.65 | 4.77 | 4.90 | 5.04 | 5.20 |
| 145 | 4.37 | 4.48 | 4.58 | 4.69 | 4.81 | 4.94 | 5.08 | 5.24 | 5.41 |
| 150 | 4.49 | 4.60 | 4.71 | 4.83 | 4.95 | 5.09 | 5.23 | 5.39 | 5.56 |
| 155 | 4.60 | 4.71 | 4.82 | 4.95 | 5.08 | 5.22 | 5.36 | 5.52 | 5.69 |
| 160 | 4.70 | 4.81 | 4.93 | 5.06 | 5.19 | 5.33 | 5.48 | 5.64 | 5.81 |
| 165 | 4.80 | 4.92 | 5.04 | 5.17 | 5.30 | 5.45 | 5.60 | 5.76 | 5.92 |
| 170 | 4.92 | 5.03 | 5.16 | 5.29 | 5.43 | 5.57 | 5.72 | 5.88 | 6.04 |
| 175 | 5.04 | 5.16 | 5.29 | 5.42 | 5.57 | 5.71 | 5.87 | 6.03 | 6.20 |
| 180 | 5.19 | 5.32 | 5.44 | 5.58 | 5.73 | 5.88 | 6.04 | 6.22 | 6.39 |
| 185 | 5.37 | 5.50 | 5.63 | 5.77 | 5.92 | 6.09 | 6.26 | 6.45 | 6.65 |
| 190 | 5.59 | 5.72 | 5.86 | 6.00 | 6.16 | 6.33 | 6.53 | 6.74 | 6.97 |
| 195 | 5.85 | 5.98 | 6.13 | 6.28 | 6.45 | 6.64 | 6.85 | 7.10 | 7.38 |
| 200 | 6.15 | 6.30 | 6.45 | 6.61 | 6.79 | 7.00 | 7.25 | 7.54 | 7.89 |

Interpolate

By interpolation:

R.W Length (Landing) = 6.33 (1000) = 6330 ft

For Take-off:

Max allowable Take – off weight = 108,900 kg

Available Take – off weight = 95,000 Kg

$$W_{Avail} < W_{Max} \Rightarrow (OK)$$

Table 18-2 Runway Length Table: Aircraft Performance, Takeoff (Boeing 757-232 Series) PW 2037 Engine, 5° Flaps

| Temperature (°C) | By Airport Elevation in Meters | | | | | |
|--|--------------------------------|-------|--------|--------|--------|--------|
| | 0 m | 500 m | 1000 m | 1500 m | 2000 m | 2500 m |
| Maximum Allowable Takeoff Weight (1000 kg) | | | | | | |
| 10 | 108.9 | 108.9 | 108.9 | 108.9 | 108.9 | 106.4 |
| 12 | 108.9 | 108.9 | 108.9 | 108.9 | 108.9 | 104.9 |
| 14 | 108.9 | 108.9 | 108.9 | 108.9 | 108.8 | 103.4 |
| 16 | 108.9 | 108.9 | 108.9 | 108.9 | 107.7 | 101.9 |
| 18 | 108.9 | 108.9 | 108.9 | 108.9 | 106.4 | 100.3 |
| 20 | 108.9 | 108.9 | 108.9 | 108.9 | 105.0 | 98.6 |
| 22 | 108.9 | 108.9 | 108.9 | 108.9 | 103.4 | 97.0 |
| 24 | 108.9 | 108.9 | 108.9 | 107.9 | 101.7 | 95.3 |
| 26 | 108.9 | 108.9 | 108.9 | 106.0 | 100.0 | 93.5 |
| 28 | 108.9 | 108.9 | 108.9 | 104.1 | 98.1 | 91.7 |
| 30 | 108.9 | 108.9 | 107.5 | 102.1 | 96.1 | 89.9 |
| 32 | 108.9 | 108.9 | 105.5 | 100.0 | 94.1 | 88.0 |
| 34 | 108.9 | 108.4 | 103.4 | 97.8 | 91.9 | 86.1 |
| 36 | 108.9 | 106.5 | 101.3 | 95.6 | 89.7 | 84.1 |
| 38 | 108.9 | 104.5 | 99.0 | 93.2 | 87.4 | 82.1 |
| 40 | 104.5 | 106.5 | 96.7 | 90.8 | 85.1 | 80.0 |
| 42 | 105.3 | 99.9 | 94.1 | 88.3 | 82.7 | 77.8 |
| 44 | 103.0 | 97.3 | 91.4 | 85.7 | 80.3 | 75.6 |

Reference Factor (R):

$R = 63.8$

| Temperature (°C) | By Airport Elevation in Meters | | | | | |
|---------------------|--------------------------------|-------|--------|--------|--------|--------|
| | 0 m | 500 m | 1000 m | 1500 m | 2000 m | 2500 m |
| | Reference Factor R | | | | | |
| 10 | 52.1 | 54.8 | 58.2 | 62.7 | 68.5 | 76.1 |
| 12 | 52.2 | 54.7 | 58.2 | 62.9 | 69.1 | 77.0 |
| 14 | 52.3 | 54.8 | 58.3 | 63.2 | 69.8 | 78.2 |
| 16 | 52.4 | 54.9 | 58.6 | 63.7 | 70.6 | 79.6 |
| 18 | 52.6 | 55.2 | 59.0 | 64.4 | 71.7 | 81.2 |
| 20 | 52.8 | 55.6 | 59.6 | 65.3 | 72.9 | 82.9 |
| 22 | 53.1 | 56.2 | 60.4 | 66.3 | 74.4 | 84.9 |
| 24 | 53.5 | 56.8 | 61.4 | 67.6 | 76.0 | 87.2 |
| 26 | 53.9 | 57.6 | 62.5 | 69.1 | 78.0 | 89.6 |
| 28 | 54.5 | 58.6 | 63.8 | 70.8 | 80.1 | 92.4 |
| 30 | 55.1 | 59.7 | 65.4 | 72.8 | 82.6 | 95.3 |
| 32 | 56.0 | 61.0 | 67.1 | 75.0 | 85.3 | 98.5 |
| 34 | 56.9 | 62.4 | 69.0 | 77.5 | 88.3 | 102.0 |
| 36 | 58.0 | 64.0 | 71.2 | 80.2 | 91.6 | 105.8 |
| 38 | 59.3 | 65.7 | 73.6 | 83.3 | 95.2 | 109.9 |
| 40 | 60.7 | 67.7 | 76.2 | 86.6 | 99.1 | 114.2 |
| 42 | 62.4 | 69.8 | 79.0 | 90.2 | 103.4 | 118.8 |
| 44 | 64.2 | 72.1 | 82.1 | 94.1 | 108.1 | 123.8 |

Runway Length for Take-off:

60 \Rightarrow 2205 m

70 \Rightarrow 2599 m

63.8 \Rightarrow ??

18-3. The FAA Airport Reference Code 551

Table 18-2 Runway Length Table: Aircraft Performance, Takeoff (Boeing 757-232 Series) PW 2037 Engine, 5° Flaps (Continued)

| Weight (1000 kg) | Runway Length in Meters | | | | | | | | |
|---------------------|-------------------------|------|------|------|------|------|------|------|------|
| | 60 | 70 | 80 | 90 | 100 | 110 | 120 | 130 | 140 |
| 70 | 1247 | 1438 | 1617 | 1786 | 1951 | 2114 | 2279 | 2451 | 2632 |
| 75 | 1409 | 1630 | 1843 | 2048 | 2249 | 2448 | 2646 | 2846 | 3051 |
| 80 | 1581 | 1838 | 2096 | 2350 | 2599 | 2837 | 3062 | 3271 | 3460 |
| 85 | 1769 | 2067 | 2377 | 2688 | 2990 | 3271 | 3522 | 3731 | 3888 |
| 90 | 1975 | 2319 | 2685 | 3056 | 3414 | 3742 | 4021 | 4234 | 4364 |
| 95 | 2205 | 2599 | 3022 | 3451 | 3864 | 4239 | 4554 | 4788 | 4917 |
| 100 | 2462 | 2912 | 3388 | 3868 | 4330 | 4754 | 5117 | | |
| 105 | 2750 | 3261 | 3782 | 4301 | 4804 | 5276 | | | |
| 110 | 3074 | 3650 | 4207 | 4748 | | | | | |

(2581 m)

By interpolation

R.W Length (Take-off) = 2355 m = 7725 ft (Controls)

Since the Take-off R.W Length controls, we must take the gradient effect into consideration:

Max difference in CL Elev = 4.5 m = 14.76 ft

R.W Length = 7725 + 10(14.76) = 7873 ft

Question 4: (5 marks)

Group E: Last two digits of students numbers 80 - 99 inclusive (e.g., 1171290)

Given the fetch of 21km, wind velocity 80km/h and mean water depth of 6 meters at an inland lake, determine the maximum wave height

$$H_{max}(ft) = 0.17\sqrt{U(mph)F(miles)}$$

$$U = 80 \frac{km}{hr} = 49.71 \text{ mph}$$

$$F = 21 \text{ km} = 13.049 \text{ statute miles}$$

$$H_{max} = 0.17\sqrt{(49.71)(13.049)} = 4.33 \text{ ft}$$